# HAYNES<sup>®</sup> 25 alloy

### **Principle Features**

#### **Excellent High-Temperature Strength and Good Oxidation Resistance**

HAYNES<sup>®</sup> 25 alloy (UNS R30605) is a cobalt-nickel- chromium-tungsten alloy that combines excellent high-temperature strength with good resistance to oxidizing environments up to 1800°F (980°C) for prolonged exposures, and excellent resistance to sulfidation. It can be fabricated and formed by conventional techniques, and has been used for cast components. Other attractive features include excellent resistance to metal galling.

#### Applications

HAYNES<sup>®</sup> 25 alloy combines properties which make it suitable for a number of component applications in the aerospace industry, including parts in established military and commercial gas turbine engines. In modern engines, it has largely been replaced by newer materials such as HAYNES<sup>®</sup> 188 alloy, and, most recently, 230<sup>®</sup> alloy, which possess improved properties. Another area of significant usage for 25 alloy is as a bearing material, for both balls and races.

### **Nominal Composition**

Weight %						
Cobalt:	51 Balance					
Nickel:	10					
Iron:	3 max.					
Chromium:	20					
Molybdenum:	1 max.					
Tungsten:	15					
Manganese:	1.5					
Silicon:	0.4 max.					
Carbon:	0.1					

### **Creep and Stress Rupture Strength**

HAYNES® 25 alloy is a solid-solution-strengthened material which possesses excellent high-temperature strength. It is particularly effective for very long-term applications at temperatures of 1200 to 1800°F (650 to 980°C). It is stronger than nickel-base solid-solutionstrengthened alloys, and is the strongest of the cobalt-base materials which still have good fabrication characteristics.

	Steel Steel Steel		Approxin	Approximate Initial Stress to Produce Specified Creep in							
Tempe	erature	Creep	10 h		10	100 h		00 h 🗸 🗸			
°F	°C 🗸	%	🗸 🗸 ksi 🗸	MPa	ksi	MPa	ksi 🧹	MPa			
Steeling" Steeling"	Station States State	0.5	62 /	<i>4</i> 27	47.5	328	33.5**	231**			
1200	649	Staffar 3th a Staffar	s s 71 s	490	54	372	39.0**	269**			
Stationant Station	Station Station State	R St	82	565	69	476	57	393 🧹			
Station Stationer	Sterner States State	0.5	43	296	30.0**	207**	21.0**	145**			
1300	704	and all some	49.5	341	35	241	23.2**	160**			
The Transfer	Statement Statement State	R /	64	441	50	345	38	262			
testingues steatingues	testmann stationed statis	0.5	28	193	19.5	134	14.8**	102**			
1400	760	a star it and	32	221	21.5	148	16.2**	112**			
C. C.	and a second and	R	47.0**	324**	36	248	26	179			
Strand Strand	Straff Staff St	0.5	18.5	128	14	97	10.2**	70**			
1500	816	° " 1, ° "	20.2	139	15.5	107	12.3**	85**			
Ster Ster	Steel Steel Steel	R	34.0**	234**	24.7	170	18.1	125			
State State	Star Star Star	0.5	13.7	94	9.9	68	6.9**	48**			
1600	871	1. Str Str	15.2	105	12	83	8.9**	61**			
States States	Staff Staff Staff	R	24.0**	165**	17.5	121	12	83			
State State	Stratt State State	0.5	9.7	67	6.8	47	4.5**	31**			
1700	927	, o <sup>rd</sup> , o <b>1</b> , o <sup>rd</sup> ,	12	83	8.8	61	5.6	39			
Steffer Steffer	Shafran Shafran Shaft	R	17.3**	119**	11.8	81	7.2	🧹 50 🖌			

\*Based upon limited data

\*\*Significant extrapolation

R= Rupture

### Creep and Stress Rupture Strength Continued

Stelland Stellard	Strationer Strationer Strat		Approxi	Approximate Initial Stress to Produce Specified Creep in:							
Tempe	rature	Creep	10	h se se s	10	0 h 🦯 🦯	1,000 h				
°F	°C	%	🖉 ksi 🦯	Мра	ksi	Мра	ksi	Мра			
or testinguist testinguist	and the second section of the	0.5	6.8	47	4.5	31	2.6	18			
1800	982	1/1/	8.8	61	5.6	39	3	21			
of Strand States	er strand	R	11.8**	81**	7.2	50	4	28			
Contraction Contraction	Transfer Car	0.5	2.8	19	1.3	9	-	and the second second			
2000	1093	<u>, 1, 1</u>	3.3	23	1.4	9.7		and a start and a start			
Steel Steel 6	trat Strat Strat	R	4.5	31	2	14		- 5 <sup>44</sup> - 5 <sup>44</sup> - 5 <sup>44</sup>			

\*Based upon limited data

\*\*Significant extrapolation

R= Rupture

#### Solution-Annealed Bar\*

Station Station Station 3	terrar Station Station Station	Ар	proximate	<b>Initial Stres</b>	s to Produ	uce Rupture	e in 🧹 🧹
Tempe	erature	🖌 10 h 🗸	Street Steation Steation Steation	100 h		1,000 h	Station Station Station
🖌 °F 🖌 .	°C	🖌 ksi 🗸 🖉	MPa	ksi	MPa	🖌 ksi 🗸	MPa
1350	732	42.5	293	36.5	252	30.3	209
1400	760	39.2	270	31.5	217	24.1	166 🧹
1500	816	30.0	207	22.0	152	17.0	117
1600	871	23.0	159	16.5	114	12.0	83
1700	927	17.0	117	12.0	83	8.4	58
1800	982	11.5	79	7.5	52	5.0	34

### **Comparative Rupture Strength, Sheet**



### **Tensile Properties**

Te Tempe	est erature	0.2% Off Stre	set Yield ngth	Ultimate Tensile Strength		Elongation
<b>۴ ۴</b> کر	°C	🔨 ksi 🧹	MPa	🖉 ksi 🧹	MPa	%
RT	RT	69	476	144.5	996	54.7
1000	538	38.8	268	119	820	63.4
1200	649	37.2	256	119.3	823	54.2
1400	760	35.5	245	82.5	569	33.9
1600	871	33.5	231	46.3	319	97.8
1800	982	18.6	128	25.8	178	94.1
2000	1093	9.0	62	13.3	92	63.0

#### **Solution Heat-Treated Sheet\***

\*Limited Data

### Solution Heat-Treated Plate

Tempe	est erature	0.2% Yield S	Offset Strngth	Ultimate Tensile Strength		Elongation
°F	°C	ksi	MPa	ksi	MPa	%
RT	RT	68.7	474	145.1	1000	58.8
1000	538	38.4	265	122.1	842	71
1200	649	33.4	230	123.5	852	64.3
1400	760	34.4	237	86	593	45.7
1600	871	32	221	48.3	333	104.7
1800	982	18.7	129	27.3	188	113.7
2000	1093	9.3	64	14.5	100 🗸 🗸	97.5

#### Hot-Rolled and 2250°F (1230°C) Solution-Annealed Bar\*

Tempe	est erature	0.2% Yield S	Offset strength	Ultimate Tensile Strength		Elongation
°F /	°C	ksi	MPa	ksi	MPa	%
RT	RT	73	505	147	1015	<u>, 60 , 60 , 60 , 60 , 60 , 60 , 60 , 60</u>
1000	538	43	295	113	780	63
1200	649	43	295	105	725	49
1400	760	41	285	90	620	29 🗸 🖉
1600	871	34	235	54	370	29 🗸 🖉
1800	982	19 🖉	130	28	195	41

\*Limited Data

**RT-** Room Temperature

\*Elevated temperature tensile tests for bar were performed with a strain rate that is no longer standard. These results were from tests with a strain rate of 0.005 in./in./minute through yield and a crosshead speed of 0.5 in./minute for every inch of reduced test section from yield through failure. The current standard is to use a strain rate of 0.005 in./ in./minute though yield and a crosshead speed of 0.05 in./minute for every inch of reduced test section from yield through failure.

### Hardness and Grain Size

Form	Hardness, HRB	Typical ASTM Grain Size
Sheet / /	/ / / / 97/ / / / /	/ / / 3.5 - 5.5 / / /
Plate	99	3.5 - 5
Bar	98	3.5 - 5

All samples tested in solution-annealed condition

### **Cold-Worked Properties**

HAYNES<sup>®</sup> 25 alloy has excellent strength and hardness characteristics in the cold-worked condition. These high property levels are also evident at elevated temperature, making 25 alloy quite suitable for applications such as ball bearings and bearing races. A modest additional increase in hardness and strength can be achieved through aging of the cold-worked material.

Cold Reduction	Te: Tempe	st rature	0.2% ( Yield St	Offset trength	Ultimate Stre	e Tensile ength	Elongation
Statut Statut Calender Statut	🥖 °F 🖉	°C 🧹	🗸 ksi 🧹	MPa	ksi	MPa	× × %
States States States States States	/ 70 /	20 🗸	105	725	155	1070	6 8 41 8 8
Statement Statement Statement Statement Statement	/ 100/	540	78	540	114	785	48
Summer State 10 State State	1200	650	80	550	115	795	/ / 37 / /
and an and a set	1400	760	67	460	87	600	8
" Statement Statement Statement Statement Statement	1600	870	47	325	62	425	13
States and states and states and states	1800	980	27	185	39	270	15
" Statement Statement Statement Statement	70	20	124	855	166	1145	30
a statement statement statement statement	1000	540	107	740	134	925	29
16	1200	650	111	765	129	890	15
	1400	760	86	595	104	715	5
and an	1600	870	52	360	70	485	/ / / / /
	1800	980	30	205	40	275	5
and the second	70	20 🗸	141	970	183	1260	19
State State State State State	1000	540	133	915	156	1075	18
20	1200	650	120	825	137	945	2
	1400	760	96	660	107	740	3 <sup>1</sup> , 3 <sup>1</sup> , 3 <sup>1</sup> , 3 <sup>1</sup> , 3 <sup>1</sup>
Station Station Station Station	1800	980	30	205	41	285	3 <sup>44</sup> 3 <sup>44</sup> 4 <sup>44</sup> 3 <sup>44</sup> 3 <sup>44</sup>

### Typical Tensile Properties, Cold-Worked Sheet\*

\*Limited data for cold-rolled 0.050-inch (1.3 mm) thick sheet

### **Cold-Worked Properties Continued**

Condition	Te Tempe	st erature	0.2% Yield S	Offset trength	Ulti Tensile	imate Strength	Elongation
and and and a set	°F	°C	ksi	MPa	ksi	MPa	%
	70	20	136	940	168	1160	31
15% CW + Age A	1200	650	104	715	128	885	23
CT CT CT CT CT CT C	70	20	152	1050	181	1250	17
	1000	540	129	890	151	1040	19
	1200	650	128	885	144	995	8
20% CVV + Age A	1400	760	97	670	108	745	2, 2
	1600	870	59	405	74	510	6, 4
Starting Starting Starting Starting Starting Starting	1800	980	33	230	43	295	5 4
State State State State State State	70	20	162	1115	191	1315	16 🗸 🗸
	600	315	132	910	165	1140	28 🗸 🗸
	1000	540	124	855	149	1025	🧹 🧹 23 🧹 🧹
20% CW + Age B	1200	650	119	820	140	965	/ / 13 / /
	1400	760	92	635	116	800	out out 7 out of
	1600	870	50	345	71	490	9
	1800	980	31	215	42	290	12

#### Typical Tensile Properties, Cold-Worked and Aged Sheet\*

\*Limited data for cold-rolled 0.050-inch (1.3 mm) thick sheet.

Age A = 700°F (370°C)/1 hour

Age B =  $1100^{\circ}$ F (595°C)/2 hours

### Typical Hardness at 70°F (20°C), Cold-Worked and Aged Sheet\*

Santan Santan Santan Santan Santan Santan Santan	Hardness Rockw	ell C, After Indicated Le Subsequent Aging Treat	vel of Cold Work and ment
Cold-Work		900°F (480°C)	1100°F (595°C)
%	None	5 h	5 h
None	24	25	25
5	31	33	31
10	37	39	39
15	40	44	43 43 4
20 20	44	44	47 5 5

\*Limited data for cold-rolled 0.070-inch (1.8 mm) thick sheet.

### **Impact Strength**

Test Tem	perature	Typical Charpy V-Notch	Impact Resistance
°F,	°C /	ftlbs.	and and and James and and
-321	-196	109	148
-216	-138	134	182
-108	-78	156	212
-20	-29	179	243
RT	RT	193	262
500	260	219	297
1000	540	201	273
1200	650	170	230
1400	760	143	194
1600	870	120	163
1800	980	106	144

#### **Impact Strength Properties, Plate**

### **Thermal Stability**

When exposed for prolonged periods at intermediate temperatures, HAYNES<sup>®</sup> 25 alloy exhibits a loss of room temperature ductility in much the same fashion as some other solid-solution-strengthened superalloys, such as HASTELLOY<sup>®</sup> X alloy or alloy 625. This behavior occurs as a consequence of the precipitation of deleterious phases. In the case of a 25 alloy, the phase in question is  $Co_2W$  laves phase. HAYNES<sup>®</sup> 188 alloy is significantly better in this regard than 25 alloy; however, for applications where thermal stability is important, 230<sup>®</sup> alloy is an even better selection.

Exposure Temperature		Exposure Time	0.2% Offset Yield Strength		Ultimate Stre	e Tensile ngth	Elongation	
°F	°C	h h	ksi	MPa	ksi 🗸	MPa	× × % × ×	
None		0	66.8	460	135	930	48.7	
Station Station S	france Staffan Staffan	500	70.3	485	123.6	850	39.2	
1200	650	1000	92.3	635	140	965	24.8	
	and start for	2500	95.1	655	130.7	900	12	
1400	760	100	68.9	475	115.3	795	18.1	
a defining defining	Starter Statement Statement	100	72.1	495	113.6	785	9.1	
1600	870	500	77.3	535	126.1	870	3.5	
	Gr Gr	1000	81.7	565	142	980	5	

#### Room-Temperature Properties of Sheet After Thermal Exposure\*

\*Composite of multiple sheet lot tests

# **Physical Properties**

Physical Property	/ / Briti	sh Units 🧹 🧹 🗸	Met	ric Units 🕢 🗸 🗸
Density	RT	0.327 lb/in <sup>3</sup>	RT	9.07 g/cm <sup>3</sup>
Melting Range	2425-2570°F	and stand stand and stand stand	1330-1410°C	and stand stand to an an an and
And	RT	34.9 µohm-in	RT	88.6 µohm-cm
and the state of t	200°F	35.9 µohm-in	100°C	91.8 µohm-cm
a a a a a a a a a a a a a a a a a a a	400°F	37.6 µohm-in	200°C	95.6 µohm-cm
and an	600°F	38.5 µohm-in	300 °C	97.6 µohm-cm
	800°F	39.1 µohm-in	400 °C	98.5 µohm-cm
Electrical	1000°F	40.4 µohm-in	500 °C	100.8 µohm-cm
Resistivity	1200°F	41.8 µohm-in	600 °C	104.3 µohm-cm
State State State State State State State	1400°F	42.3 µohm-in	700 °C	106.6 µohm-cm
and and a star and and and and	1600°F	40.6 µohm-in	800 °C	107.8 µohm-cm
and and an an an an an	1800°F	37.7 µohm-in	900 °C	101.1 µohm-cm
Staff Staff Staff Staff Staff Staff Staff	and and a state of the state of	1 dr. dr. d <u>r</u> . dr. <del>1</del> dr.	1000 °C	95.0 µohm-cm
State State State State State State	70°F	4.4 x 10 <sup>-3</sup> in <sup>2</sup> /sec	RT	28.3 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
States States States States States States	125°F	4.6 x 10 <sup>-3</sup> in <sup>2</sup> /sec	100°C	30.1 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
States States States States States States	200°F	4.8 x 10 <sup>-3</sup> in <sup>2</sup> /sec	200°C	32.7 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
	400°F	5.5 x 10 <sup>-3</sup> in <sup>2</sup> /sec	300°C	35.6 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
Stand Stand Stand Stand Stand	600°F	6.0 x 10 <sup>-3</sup> in <sup>2</sup> /sec	400°C	41.2 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
Thermal	800°F	6.5 x 10 <sup>-3</sup> in <sup>2</sup> /sec	500°C	43.5 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
Diffusivity	1000°F	6.9 x 10 <sup>-3</sup> in <sup>2</sup> /sec	000°C	45.5 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
Stand Stand Stand Stand Stand	1200°F	7.3 x 10 <sup>-3</sup> in <sup>2</sup> /sec	700°C	47.6 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
Alter and alter alter alter alter alter alter	1400°F	7.6 x 10 <sup>-3</sup> in <sup>2</sup> /sec	800°C	49.6 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
Anteren Anteren Anteren Anteren Anteren	1600°F	7.7 x 10 <sup>-3</sup> in <sup>2</sup> /sec	900°C	48.7 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
a statement at a statement at a statement at a statement at a statement	1800°F	7.9 x 10 <sup>-3</sup> in <sup>2</sup> /sec	1000°C	51.6 x 10 <sup>-3</sup> cm <sup>2</sup> /sec
a a a a a a a a a a a a a a a a a a a	2000°F	8.3 x 10 <sup>-3</sup> in <sup>2</sup> /sec	the second s	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	70°F	72 Btu-in/ft <sup>2</sup> -h-°F	25°C	10.5 W/m-°C
	125°F	77 Btu-in/ft <sup>2</sup> -h-°F	100°C	12.0 W/m-°C
	200°F	83 Btu-in/ft <sup>2</sup> -h-°F	200°C	14.0 W/m-°C
	400°F	99 Btu-in/ft <sup>2</sup> -h-°F	300°C	15.9 W/m-°C
	600°F	114 Btu-in/ft <sup>2</sup> -h-°F	400°C	17.7 W/m-°C
Thermal	800°F	127 Btu-in/ft <sup>2</sup> -h-°F	500°C	19.5 W/m-°C
Conductivity	1000°F	140 Btu-in/ft <sup>2</sup> -h-°F	600°C	21.2 W/m-°C
and and a star and a star and a star and a star	1200°F	152 Btu-in/ft <sup>2</sup> -h-°F	700°C	22.9 W/m-°C
and an are an are an are	1400°F	165 Btu-in/ft <sup>2</sup> -h-°F	800°C	24.5 W/m-°C
and and and and and	1600°F	178 Btu-in/ft <sup>2</sup> -h-°F	900°C	26.0 W/m-°C
State State State State State State	1800°F	191 Btu-in/ft <sup>2</sup> -h-°F	1000°C	27.5 W/m-°C
State State State State State State	2000°F	201 Btu-in/ft <sup>2</sup> -h-°F	State State - State State State	and share share share share share share

RT- Room Temperature

# Physical Properties Continued

Physical Property	Britis	h Units	Metric	Units / / /
State State State State State State State	70°F	0.096 Btu/lb°F	25°C	403 J/kg-°C
and a second stand and a second stand stand	125 °F	0.098 Btu/lb°F	100 °C	424 J/kg-°C
and a start of the	200 °F	0.101 Btu/lb°F	200 °C	445 J/kg-°C
and the state of t	400 °F	0.106 Btu/lb°F	300 °C	455 J/kg-°C
Specific Heat	600°F	0.111 Btu/lb°F	400 °C	462 J/kg-°C
	800 °F	0.116 Btu/lb°F	500 °C	495 J/kg-°C
Specific fieat	1000 °F	0.119 Btu/lb°F	600 °C	508 J/kg-°C
and and a set and a set of the se	1200 °F	0.123 Btu/lb°F	700 °C	582 J/kg-°C
and and an and an and an and and and and	1400 °F	0.128 Btu/lb°F	800 °C	592 J/kg-°C
and	1600 °F	0.137 Btu/lb°F	900 °C	596 J/kg-°C
and a star and a star and a star and a star a st	1800 °F	0.143 Btu/lb°F	1000 °C	598 J/kg-°C
and a set of the set o	2000 °F	0.142 Btu/lb°F		a di santa anta anta anta anta anta anta ant
Start Start Start Start Start Start Start	70 - 200 °F	7.1 µin/in°F	25 - 100 °C	12.8 µm/m-°C
States States States States States States States	70 - 400 °F	7.3 µin/in°F	25 - 200 °C	13.1 µm/m-°C
States States States States States States	70 - 600 °F	7.5 µin/in°F	25 - 300 °C	13.3 µm/m-°C
States States States States States States States	70 - 800 °F	7.7 µin/in°F	25 - 400 °C	13.7 µm/m-°C
Mean Coefficient of	70 - 1000 °F	7.9 µin/in°F	25 - 500 °C	14.0 µm/m-°C
Thermal Expansion	70 - 1200 °F	8.2 μin/in°F	25 - 600 °C	14.6 µm/m-°C
a statement statement statement statement statement state	70 - 1400 °F	8.6 µin/in°F	25 - 700 °C	15.1 µm/m-°C
. Stand Stand Stand Stand Stand Stand Stand	70 - 1600 °F	<mark>8.</mark> 9 μin/in°F	25 - 800 °C	15.8 µm/m-°C
and the state of t	70 - 1800 °F	9.2 µin/in°F	25 - 900 °C	16.2 µm/m-°C
a and a support and a support and a support and a support	70 - 2000 °F	9. <mark>5 µ</mark> in/in°F	25 - 1000 °C	16.7 µm/m-°C
and the state of t	RT	32.6 x 10 <sup>6</sup> psi	RT	225 GPa
a construction and a construction and a construction of the	200°F	32.3 x 10 <sup>6</sup> psi	100°C	222 GPa
a stand stand stand stand stand	400°F	31.0 x 10 <sup>6</sup> psi	200°C	214 GPa
	600°F	29.4 x 10 <sup>6</sup> psi	300°C	204 GPa
Dynamic Modulus	800°F	28.3 x 10 <sup>6</sup> psi	400°C	197 GPa
of Elasticity	1000°F	26.9 x 10 <sup>6</sup> psi	500°C	188 GPa
	1200°F	25.8 x 10 <sup>6</sup> psi	600°C	181 GPa
and and a set of a set of a	1400°F	24.3 x 10 <sup>6</sup> psi	700°C	174 GPa
State State State State State State	1600°F	22.8 x 10 <sup>6</sup> psi	800°C	163 GPa
States States States States States States States	1800°F	21.4 x 10 <sup>6</sup> psi	900°C	154 GPa
and a star and a star and a star and		Statement Statement Statement Statement Statement	1000°C	146 GPa

**RT- Room Temperature** 

### Wear Resistance

HAYNES 25 alloy exhibits excellent resistance to metal galling and cavitation. Metal-to-Metal Galling results shown below were generated for standard matching material roomtemperature pin on disc tests. Wear depths are given as a function of applied load. Cavitation tests were performed in accordance with ASTM G 32 water at 16°C, with a frequency of 20 kHz and an amplitude of 0.05 mm. The results of the wear tests indicate that 25 alloy is superior in galling and cavitation resistance to many materials, and is surpassed only by ULTIMET® alloy and HAYNES 6B alloy. Both of these materials were specifically designed to have excellent wear resistance.

Charles Charles Charles Charles Charles Charles	Gall	Galling - Degree of Damage for Various Applied Loads									
Alloy	3,000 lbs.	(1,365 kg)	6,000 lbs.	(2,725 kg)	9,000 lbs.	9,000 lbs. (4,090 kg)					
alterna alterna alterna alterna	mils	μm	mils	μm	mils	μm					
6B	0.02	0.6	0.03	0.7	0.02	0.5					
ULTIMET®	0.11	2.9	0.11	2.7	0.08	2					
25	0.23	5.9	0.17	4.2	0.17	4.2					
188	1.54	39.2	3.83	97.3	3.65	92.6					
HR-160 <sup>®</sup>	1.73	43.9	4.33	109.9	3.81	96.8					
214 <sup>®</sup>	2.32	59	3.96	100.5	5.55	141					
<b>556</b> ®	3.72	94.4	5.02	127.6	5.48	139.3					
230 <sup>®</sup>	4.44	112.7 🧹	7.71	195.8	8.48	215.5					
HR-120 <sup>®</sup>	6.15	156.2	7.05	179	10.01	254.2					

a contraction and provide a state of the	Cavitation - Mean Depth of Erosion											
Alloy	2	24 h		48 h		72 h		6 h 🦯 🖊				
Start Start Start Start	mils	μm	mils	μm	mils	μm	mils	μm				
ULTIMET®	0.3	6.8	0.9	22.9	1.6	40.2	2.3	57.4				
,	0.3	7.7	0.9	22.3	1.4	34.8	1.9	48				
25 🗸 🗸	State 1 State	24.4	2.1	53.6	3.4	85.6	4.5	115.1				
625 /	3.1	80	7	176.6	10.2	259.2	Not tested	Not Tested				
<b>556<sup>®</sup></b>	3.3	83.8	6.9	175.8	9.6	244.3	11.4	289.8				
230 <sup>®</sup>	3.8	97.6>	7.5	190.1	9.9	251.8	11.9	301.7				

Tested in accordance with ASTM G 32 water at 16°C, with a frequenct of 20 kHz and an amplitude of 0.05 mm

### **High-Temperature Hardness**

The following are results from standard vacuum furnace hot hardness tests. Values are given in originally measured DPH (Vickers) units and conversions to Rockwell C/B scale.

	100 100			101 IN 101	191 (B)	191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191	1997 - 19	1 (B) (B)	197 - 197 - 197	18 <sup>1</sup>		
an an an an an an	3° - 3°	Vickers Diamond Pyramid Hardness (Rockwell C/B Hardness)										
Staffer Staffer Staffer Staffer Staffer	70°I	F (20°C)	800°F	<sup>=</sup> (425°C)	1000°F	<sup>=</sup> (540°C)	1200°F	(650°C)	1400°F	(760°C)		
Solution Treated	251	22 HRC	171	87 HRC	160	83 HRB	150	80 HRB	134	74 HRB		
15% Cold Work	348	35 HRC	254	23 HRC	234 🖉	97 HRB	218	95 HRB	or Sheller Sheller	States - States St		
20% Cold Work	401	41 HRC	318	32 HRC	284	27 HRC	268	25 HRC	one Station Station	Station Station Str		
25% Cold Work	482	48 HRC	318	32 HRC	200	30 HRC	286	28 HRC	one States States	Station Station St		

HRB = Hardness Rockwell "B". HRC = Hardness Rockwell "C".

### **Aqueous Corrosion Resistance**

States States States States	Average Corrosion Rate, per year										
Alloy	1% HCI	(Boiling)	10% H <sub>2</sub> SO	(Boiling)	65% HNO <sub>3</sub> (Boiling)						
Station Station - Station Station	mils	🧹 .mm 🧹	🧹 mils 🧹	🖉 🦛 🧹	🧹 mils 🧹	🖉 mm 🧹					
<b>ULTIMET</b> ®	/ /<1/	<0.03 🧹	99 🖉	2.51	6 / 6	0.15 🧹					
<b>C-22<sup>®</sup></b>	J 3 J 3	0.08	J J12	0.3	134	3.4					
25	226	5.74	131	3.33	31	0.79					
Type 316L	524	13.31	1868	47.45	9	0.23					

HAYNES<sup>®</sup> 25 alloy was not designed for resistance to corrosive aqueous media. Representative average corrosion data are given for comparison. For applications requiring corrosion resistance in aqueous environments, ULTIMET<sup>®</sup> alloy and HASTELLOY<sup>®</sup> corrosion-resistant alloys should be considered.

### **Oxidation Resistance**

HAYNES<sup>®</sup> 25 alloy exhibits good resistance to both air and combustion gas oxidizing environments, and can be used for long-term continuous exposure at temperatures up to 1800°F (980°C). For exposures of short duration, 25 alloy can be used at higher temperatures. Applications for which oxidation resistance is a serious consideration normally call for newer, more capable materials such as 230<sup>®</sup> alloy or HAYNES<sup>®</sup> 188 alloy. This is particularly important at temperatures above 1800°F (980°C).



- 1. Metal Loss = (A B)/2
- 2. Average Internal Penetration = C
- 3. Maximum Internal Penetration = D
- 4. Average Metal Affected = ((A B)/2) + C
- 5. Maximum Metal Affected = ((A B)/2) + D

#### Comparative Burner Rig Oxidation Resistance 1000 Hour Exposure at 1800°F (980°C)

Strand States Strand St	Meta	Metal Loss		etal Affected	Maximum Metal Affected					
Alloy	mils	μm	mils	/ µm / /	mils	μm				
188	1.1	28	3.2	81	3.9	99				
230®	2.8	71	5.6	142	6.4	163				
617	2.4	61	5.7	145	6.9	175				
625	3.7	94	6	152	6.6	168				
, or X or , or	4.3	109	7.3	185	8 0	203				
25	7.8	198	9.8	249	10.3	262				
310SS	16 🧹	406	18.3	465	19.5	495				
600H	22.9	582	l 🖉 🖉 🖉 Inte	Internal oxidation through thickness						

### **Oxidation Resistance Continued**

#### **Oxidation Test Parameters**

Burner rig oxidation tests were conducted by exposing samples 3/8 in. x 2.5 in. x thickness (9 mm x 64 mm x thickness), in a rotating holder, to products of combustion of No. 2 fuel oil burned at a ratio of air to fuel of about 50:1. (Gas velocity was about 0.3 mach). Samples were automatically removed from the gas stream every 30 minutes and fancooled to near ambient temperature and then reinserted into the flame tunnel.

Testimore Sectionality Steel	a station station	1800°F (9	2	2000°F (1095°C)				2100°F (1150°C)					
Alloy	Average Metal Affected**		Average Metal Loss		Averag Affec	Average Metal Affected**		Average Metal Loss		Average Metal Affected**		Average Metal Loss	
Star Star Star	mils	μm	mils	μm	mils	μm	mils	μm	mils	μm	mils	μm	
188	1.1	28	0.1	3	3.7	94	0.5	13	10.7	272	8.6	218	
230 <sup>®</sup>	1.5	38	0.2	5	3.3	84	0.5	13	4.4	112	1.2	30	
25 🗸	2	51 🖉	0.3	J 8	10.2	259	9.2	234	10.7	272	8.2	208	
34" X 34	1.5	38 🧹	0.2	5	4.4	112	1.3	33	6.1	115	3.6	91	
625	1.9	48	0.4	10	7.8	198	3.5	89	20.2	513	18.3	465	
617	2	51 /	0.3	8	3.8	97	0.6	15	5.2	132	Jarran 1 Jarran	25	
800HT	4.1	/ 104 /	0.5	13	11.6	295	7.6	193	15	381	_11_	279	

#### **Comparative Oxidation Resistance in Flowing Air\***

\* Flowing air at a velocity of 7.0 ft./min. (213.4 cm/min.) past the samples. Samples cycled to room temperature once-a-week.

\*\* Metal Loss + Average Internal Penetration.

#### Comparative Burner Rig Oxidation Resistance at 2000°F (1095°C) for 500 Hours

Alloy	Average Meta	Loss per Side	Maximum Metal Affected		
Setting Setting Stands	mils	μm	mils	μm	
214®	1.2	30.5	1.8	45.7	
230®	7.1	180.3	/ 11.8	299.7	
188	10.9	276.9	14.1	358.1	
X	11.6	294.6	15.1	383.5	
25	> 25*	>635*		10 50 50 50 50 50 10 10 10 10 10 10 10 10 10 10 10 10 10 1	

\*> 25 mils (63<mark>5 µm)</mark> in 1<mark>65 h</mark>ours

### **Sulfidation Resistance**

### Sulfidation Resistance at 1400°F (760°C)

HAYNES<sup>®</sup> 25 alloy has very good resistance to gaseous sulfidation environments encountered in various industrial applications. Tests were conducted at 1400°F (760°C) in a gas mixture consisting of 5 percent H<sub>2</sub>, 5 percent CO, 1 percent CO<sub>2</sub>, 0.15 percent H<sub>2</sub>S and 0.1 percent H<sub>2</sub>O, balance Ar. Coupons were exposed for 215 hours. This is a severe test, with equilibrium sulfur partial pressure of 10-6 to 10-7 and oxygen partial pressures less than that needed to produce protective chromium oxide scales.

### **Sulfidation Resistance Continued**



#### Schematic Representation of Metallographic Technique Used for Evaluating Environmental Tests



1. Metal Loss = (A - B)/2

- 2. Average Internal Penetration = C
- 3. Maximum Internal Penetration = D
- Average Metal Affected = ((A B)/2) + C
- 5. Maximum Metal Affected = ((A B)/2) + D

### Fabrication

HAYNES<sup>®</sup> 25 alloy has good forming and welding characteristics. It may be forged or otherwise hot-worked, providing that it is held at 2200°F (1205°C) for a time sufficient to bring the entire piece to temperature. The alloy has good ductility, and thus also may be formed by cold working. The alloy does work-harden very rapidly, however, so frequent intermediate annealing treatments will be needed for complex component forming operations. All hot- or cold-worked parts should be annealed and rapidly cooled in order to restore the best balance of properties. The alloy can be welded by both manual and automatic welding methods, including gas tungsten arc (GTAW), gas metal arc (GMAW), shielded metal arc, electron beam and resistance welding. It exhibits good restraint welding characteristics.

### **Fabrication Continued**

#### **Heat Treatment**

HAYNES<sup>®</sup> 25 alloy is furnished in the solution heat-treated condition, unless otherwise specified. The alloy is normally final solution heat-treated at 2150 to 2250°F (1175 to 1230°C) for a time commensurated with section thickness and rapidly cooled or waterquenched for optimal properties. Because annealing at temperatures less than the solution heat-treating temperature will produce some carbide precipitation in 25 alloy, which may affect the alloy's properties, annealing during fabrication may be performed at lower temperatures, but a final, subsequent solution heat treatment is needed to produce optimum properties and structure.

#### Machining

For information on Machining, please refer to the machining section of Welding and Fabrication.

Cold Reduction	Subsequent Anneal	0.2% Yield S	Offset trength	Ultin Tens <mark>ile</mark> S	nate Strength	Elongation	HRC
%	and a star and a star and a star a	ksi	MPa	ksi	MPa	%	State State State
	Starting Starting Starting Starting St	68.4	470	144	995	58.5	24
10	Nono	123.6	850	181.9	1255	37.1	36 🗸
J 315 J	None	148.5	1025	178.2	1230	27.7	40 🧹
20	Statement Statement Statement Statement Statement	150.9	1040	193.5	1335	18.2	42 🧹
25	" Setter Stand Stand Stand Stand Stand	183.9	1270	232.5	1605 🧹	14.6	🧹 44 🧹
<i></i>	States States States States States	97.9	675	163	1125	39.3	/ 32 /
15	1950°F (1065°C)	91.2	630	167.1	1150	43.8	30
20	for 5 min.	96.5	665	170.7	1175	40.8	32
25	and and and and and and	88.9	615	169.5	1170	44.3	32
10		74	510	156.6	1080	53.4	27
15	2050°F (1120°C)	78.6	540	161.2	1110	51.9	28
20	for 5 min.	82	565	164.8	1135	47.6	31
25		82.9	570	165.6	1140	48	30
10		66.9	460	148.1	1020	62.6	21
15	2150°F (1117°C)	73.6	505	156.1	1075	55.4	26
20	for 5 min.	72.1	495	154	1060	59.3	26
25		68.5	470	149.3	1030	61.7	25

### Formability

\*Based upon cold reductions taken upon 0.110-inch (2.8 mm) thick sheet. Duplicate tests.

HRC = Hardness Rockwell "C".

### Welding

HAYNES<sup>®</sup> 25 alloy is readily welded by Gas Tungsten Arc (GTAW), Gas Metal Arc (GMAW), Shielded Metal Arc (SMAW), electron bean welding, and resistance welding techniques. Its welding characteristics are similar to those of HAYNES<sup>®</sup> 188 alloy. Submerged Arc welding is not recommended, as this process is characterized by high heat input to the base metal and slow cooling of the weld. These factors can increase weld restraint and promote cracking.

#### **Base Metal Preparation**

The joint surface and adjacent area should be thoroughly cleaned before welding. All grease, oil, crayon marks, sulfur compounds, and other foreign matter should be removed. Contact with copper or copper-bearing materials in the joint area should be avoided. It is preferable, but not necessary, that the alloy be in the solution-annealed condition when welded.

#### **Filler Metal Selection**

Matching composition filler metal is recommended for joining alloy 25. For shielded metal arc welding, HAYNES<sup>®</sup> 25 alloy electrodes (AMS 5797) are suggested. For dissimilar joining of 25 alloy to nickel-, cobalt-, or iron- base materials, 25 alloy itself (AMS 5796), 230-W<sup>®</sup> filler wire(AMS 5839), HAYNES<sup>®</sup> 556<sup>®</sup> alloy (AMS 5831), HASTELLOY<sup>®</sup> S alloy (AMS 5838), or HASTELLOY<sup>®</sup> W alloy (AMS 5786) welding products are suggested, depending upon the particular case. Please see the "Welding and Fabrication" brochure or the Haynes Welding SmartGuide for more information.

#### Preheating, Interpass Temperatures, and Post-Weld Heat Treatment

Preheat is not required. Preheat is generally specified as room temperature (typical shop conditions). Interpass temperature should be maintained below 200°F (93°C). Auxiliary cooling methods may be used between weld passes, as needed, providing that such methods do not introduce contaminants. Post-weld heat treatment is not generally required for 25 alloy. For further information, please consult the "Welding and Fabrication" brochure.

	0.2% Yield S	Offset trength	Ultimate Stre	Tensile ngth	Elongation	
Form	ksi	MPa	ksi	MPa	%	
Sheet	<b>6</b> 9	476	144.5	996	54.7	
Plate	68.7	474	145.1	1000	58.8	
Welded Transverse, GTAW	72.4	499	134.2	925	36.5	
All Weld Metal, SMAW	88.6	611	141	972	31.5	

#### Welded Tensile - Room Temperature

### **Specifications**

AMS 5537 AMS 5759 IL-C-24252D
AMS 5537 AMS 5759 IL-C-24252D
AMS 5759 IL-C-24252D
AMS 5797
AMS 5796
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AMS 5759
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-5031B Class 13

Codes	
HAYNES	® 25 alloy
(R3)	0605)
MMPDS	6.4.1

#### **Disclaimer:**

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